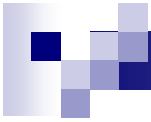
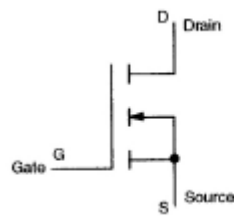
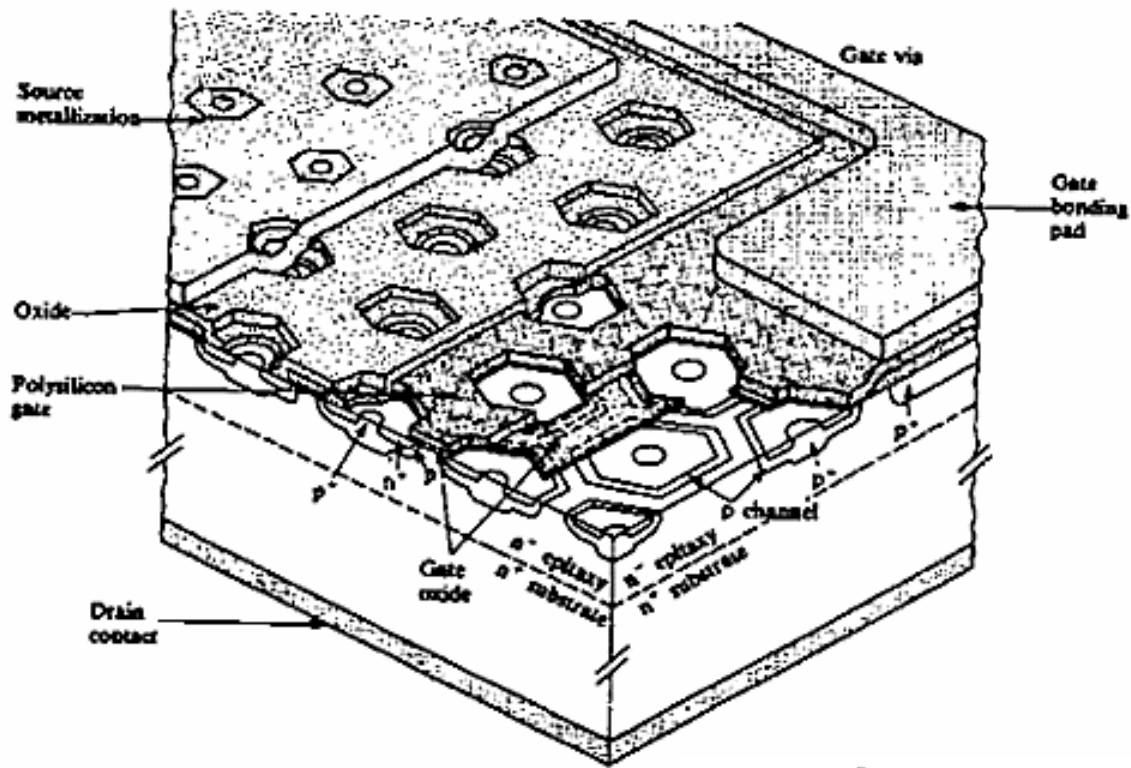


Power MOSFET

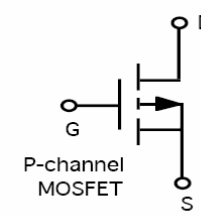
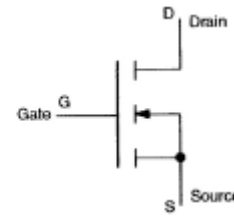




International Rectifier : ■
VMOS : ■
LSI : ■
: ■



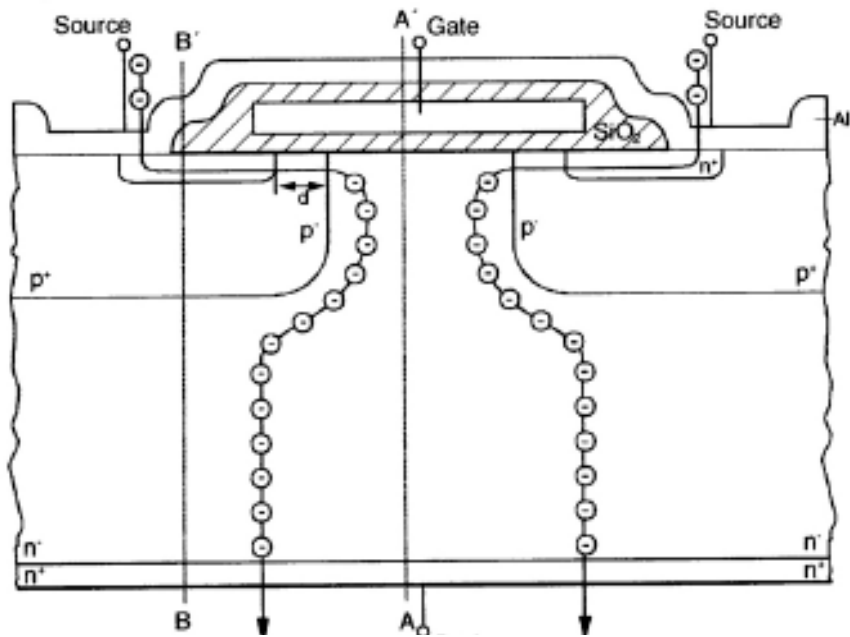
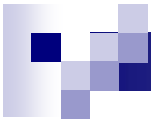
n



P-channel MOSFET

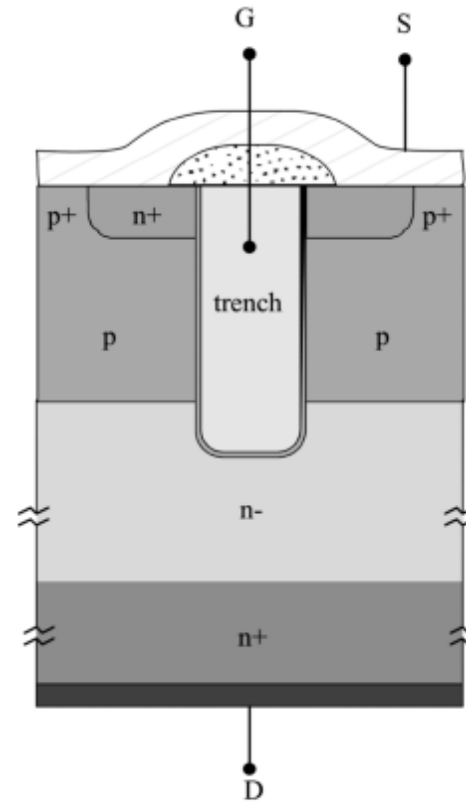
p





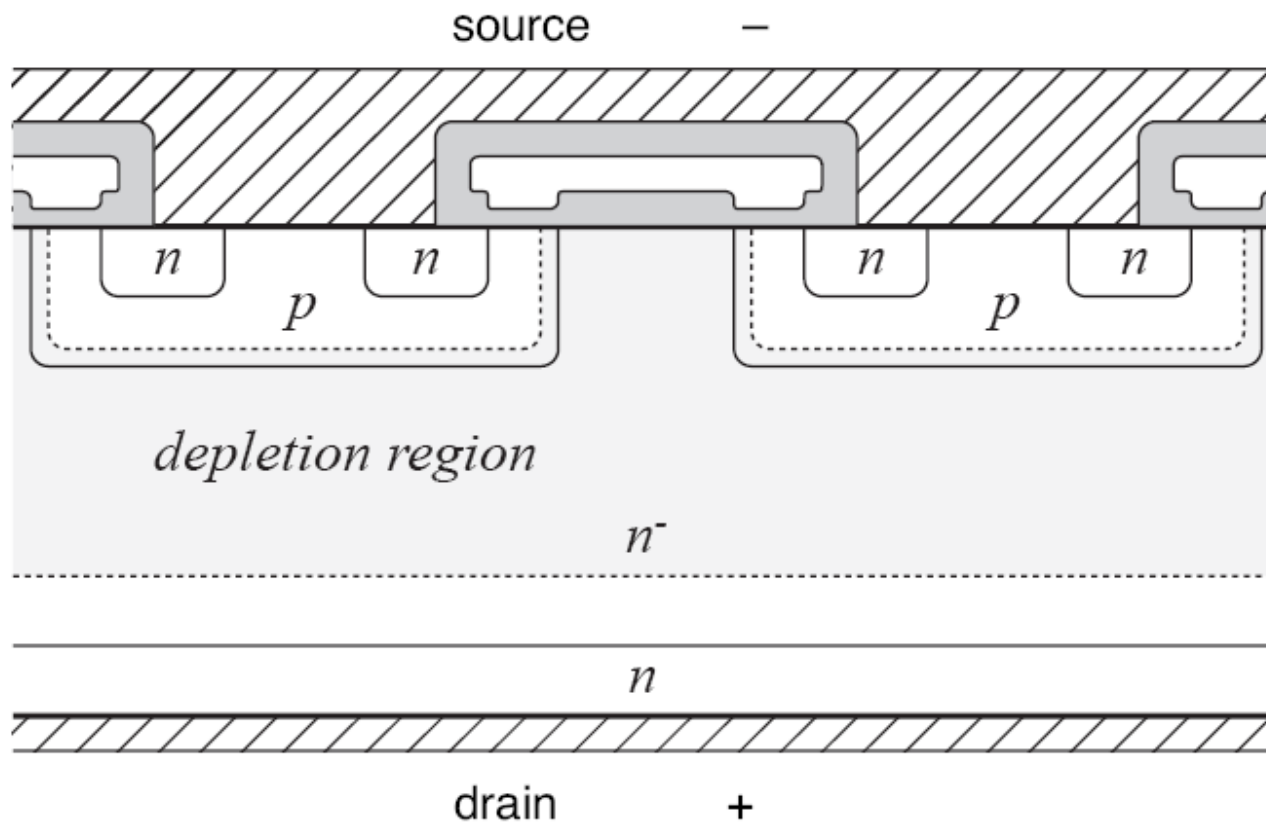
Power MOSFET (SIPMOS planar gate structure)

d: length of channel

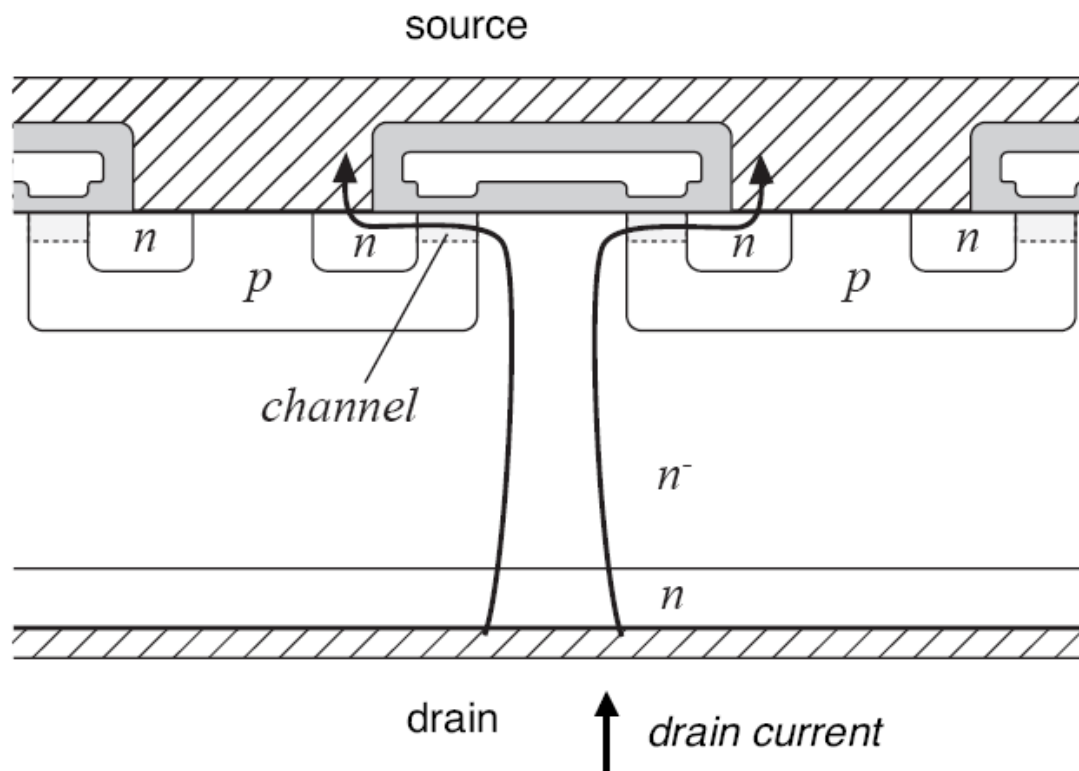


c) MOSFET with trench gate structure

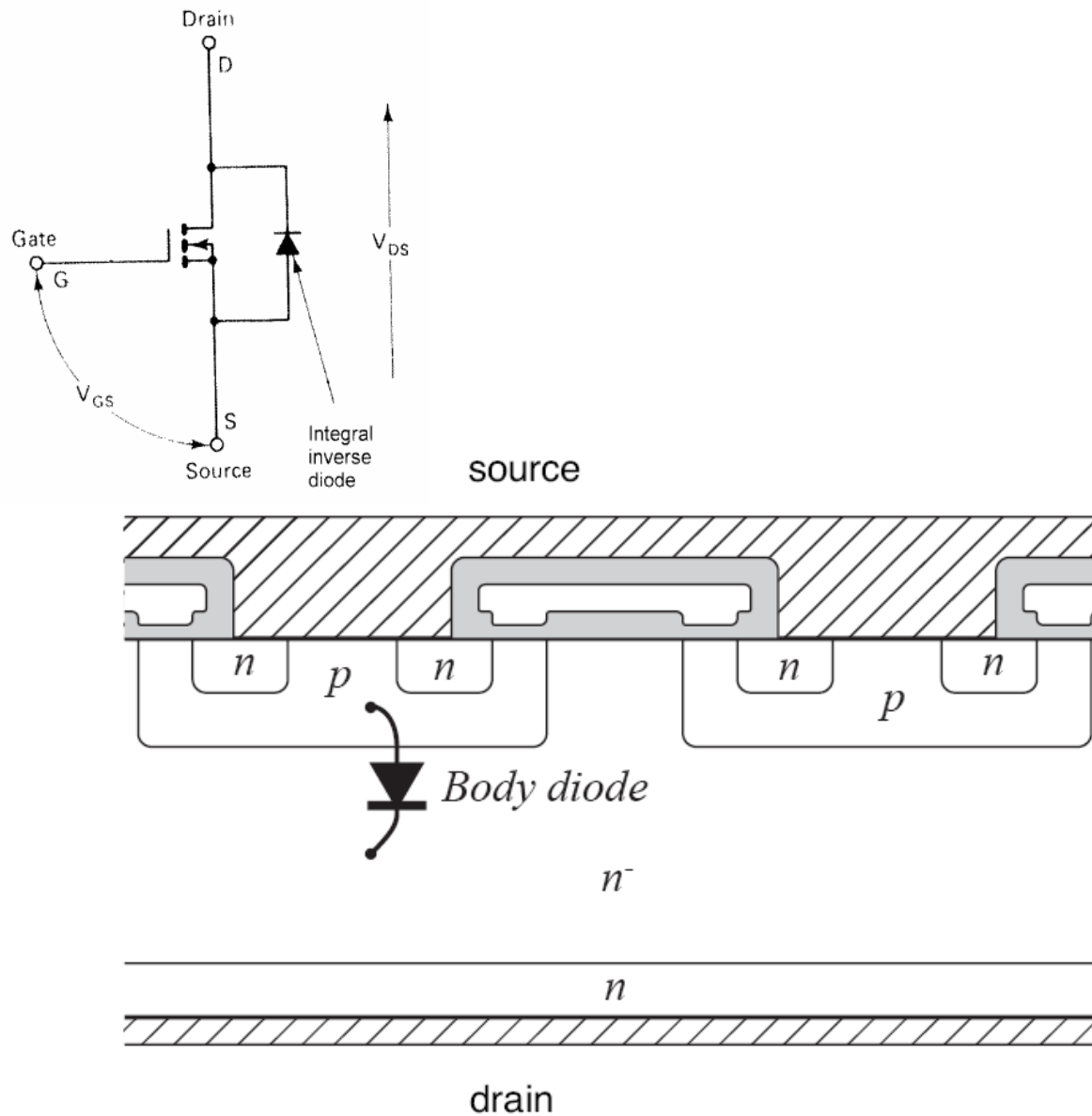
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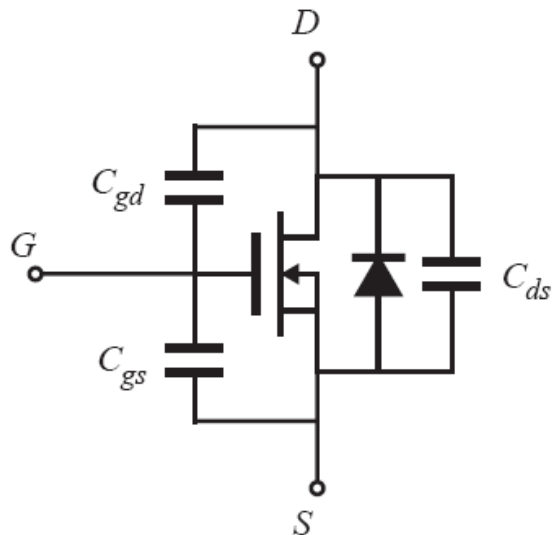
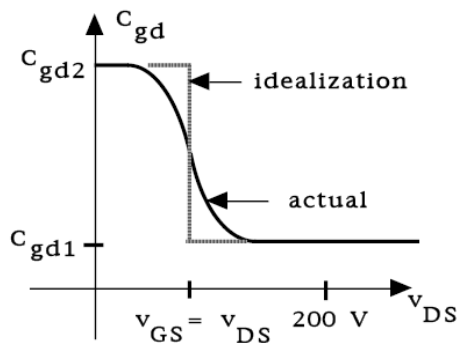
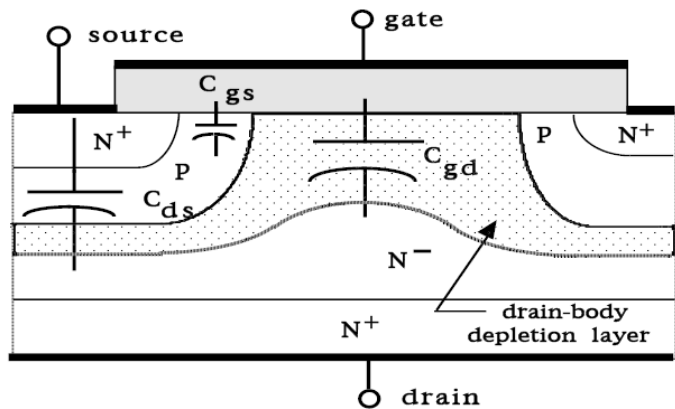
- $p-n^-$ junction is reverse-biased
- off-state voltage appears across n^- region



- $p-n$ junction is slightly reverse-biased
- positive gate voltage induces conducting channel
- drain current flows through n region and conducting channel
- on resistance = total resistances of n region, conducting channel, source and drain contacts, etc.



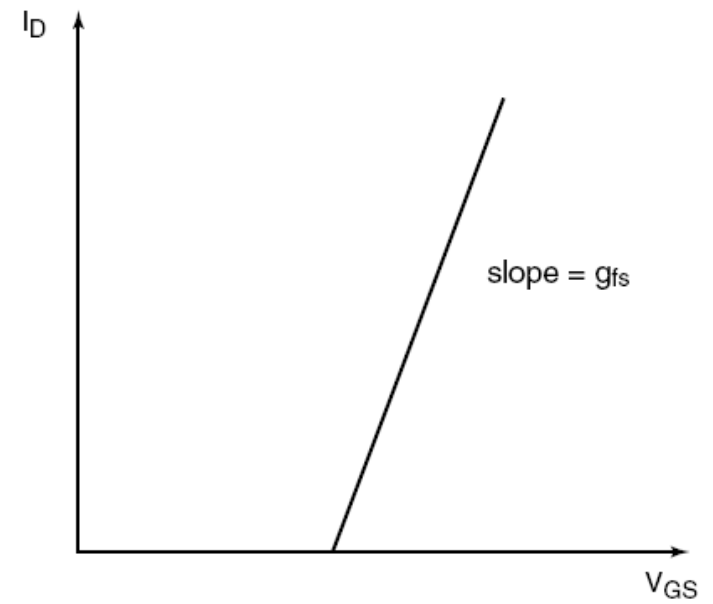
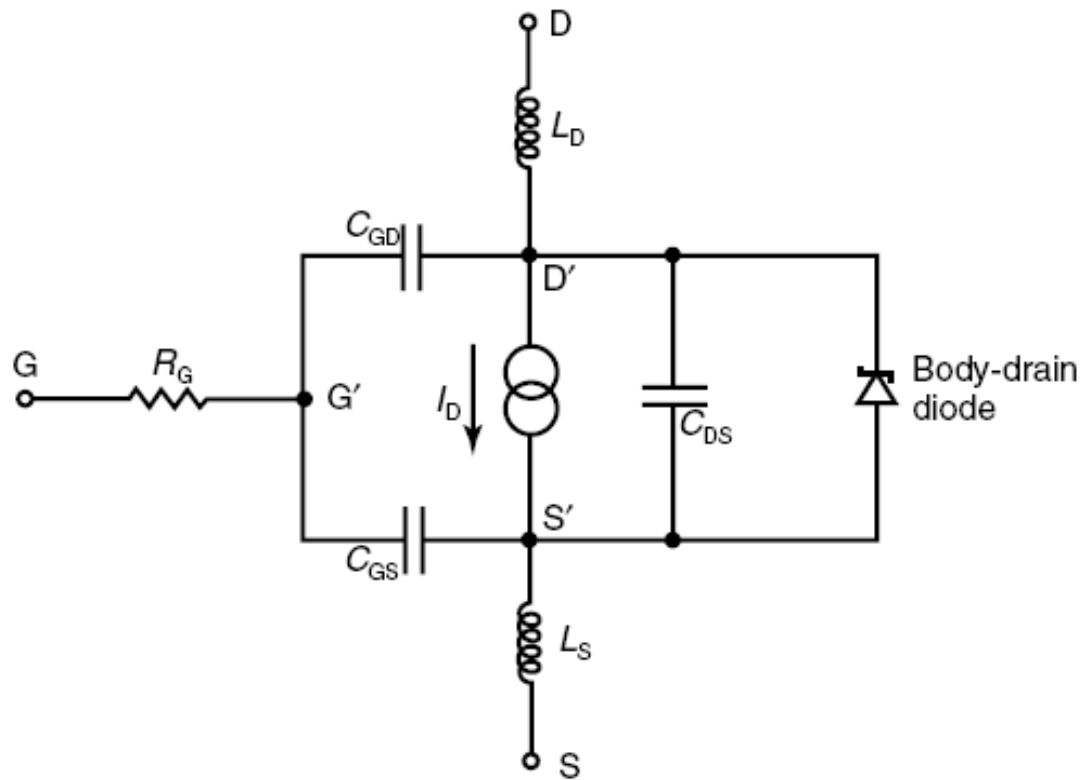
- p - n junction forms an effective diode, in parallel with the channel
- negative drain-to-source voltage can forward-bias the body diode
- diode can conduct the full MOSFET rated current
- diode switching speed not optimized — body diode is slow, Q_r is large



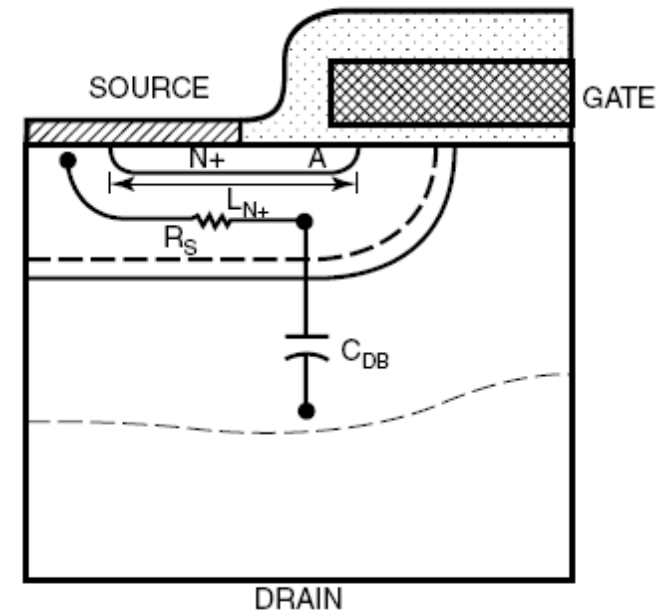
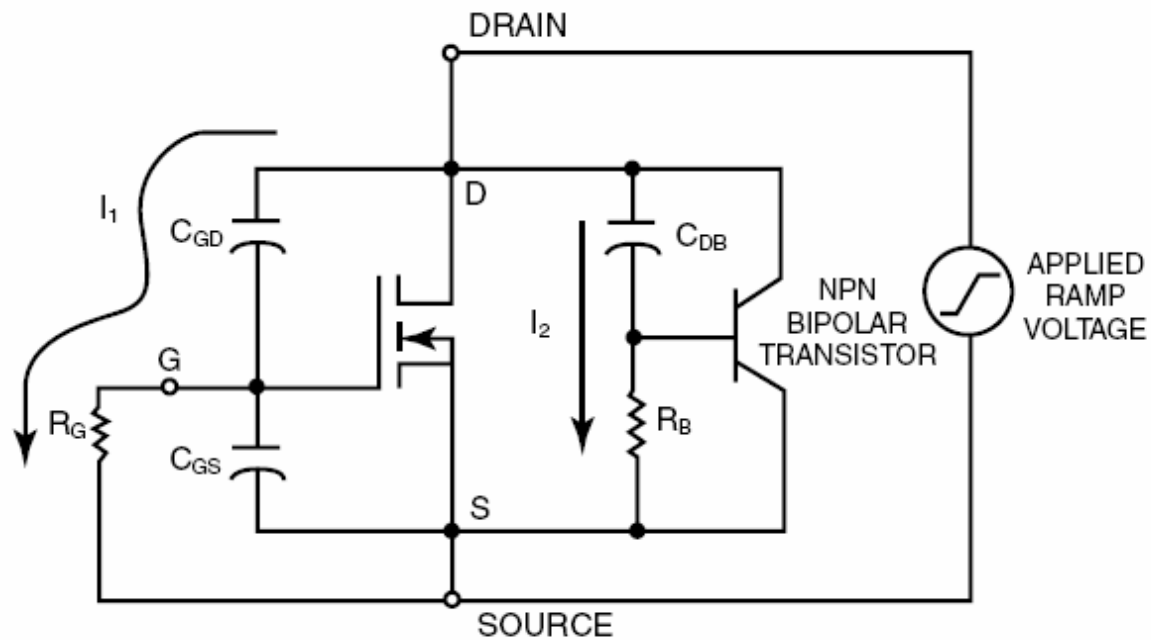
- C_{gs} : large, essentially constant
- C_{gd} : small, highly nonlinear
- C_{ds} : intermediate in value, highly nonlinear
- switching times determined by rate at which gate driver charges/discharges C_{gs} and C_{gd}

$$C_{ds}(v_{ds}) = \frac{C_0}{\sqrt{1 + \frac{v_{ds}}{V_0}}}$$

$$C_{ds}(v_{ds}) \approx C_0 \sqrt{\frac{V_0}{v_{ds}}} = \frac{C'_0}{\sqrt{v_{ds}}}$$



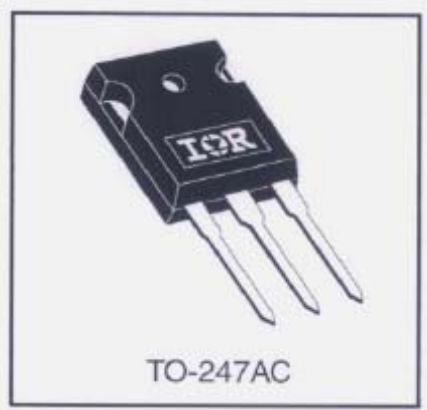
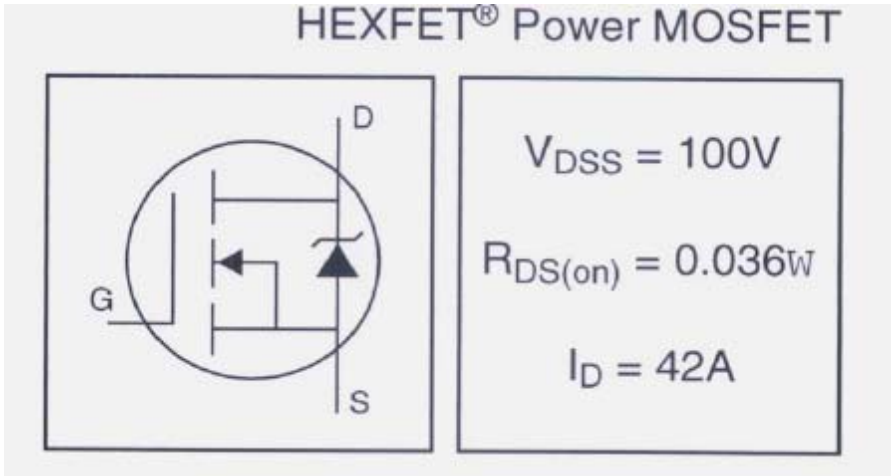
dV/dt





- A majority-carrier device: fast switching speed
- Typical switching frequencies: tens and hundreds of kHz
- On-resistance increases rapidly with rated blocking voltage
- Easy to drive
- The device of choice for blocking voltages less than 500V
- 1000V devices are available, but are useful only at low power levels (100W)
- Part number is selected on the basis of on-resistance rather than current rating

IRFP150NPbF



Absolute Maximum Ratings

	Parameter	Max.	Units
$I_D @ T_C = 25^\circ C$	Continuous Drain Current, $V_{GS} @ 10V$	42	A
$I_D @ T_C = 100^\circ C$	Continuous Drain Current, $V_{GS} @ 10V$	30	
I_{DM}	Pulsed Drain Current ①⑤	140	
$P_D @ T_C = 25^\circ C$	Power Dissipation	160	W
	Linear Derating Factor	1.1	W/°C
V_{GS}	Gate-to-Source Voltage	± 20	V

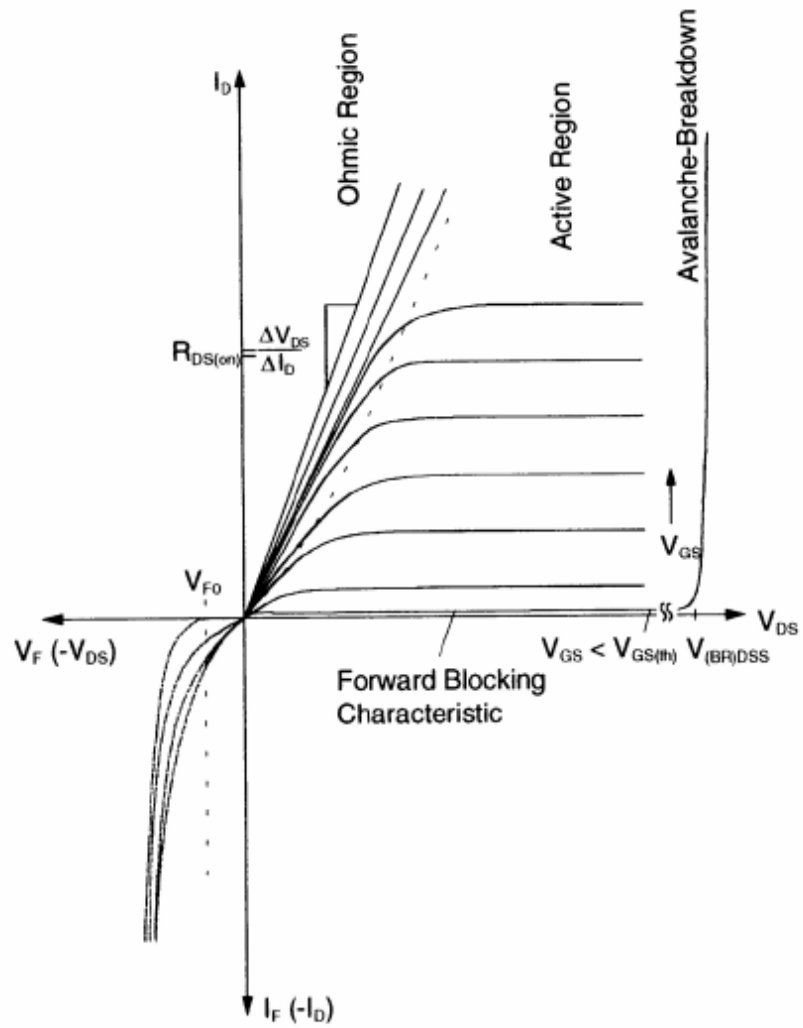


Fig. 3 a) Output characteristic of MOSFETs

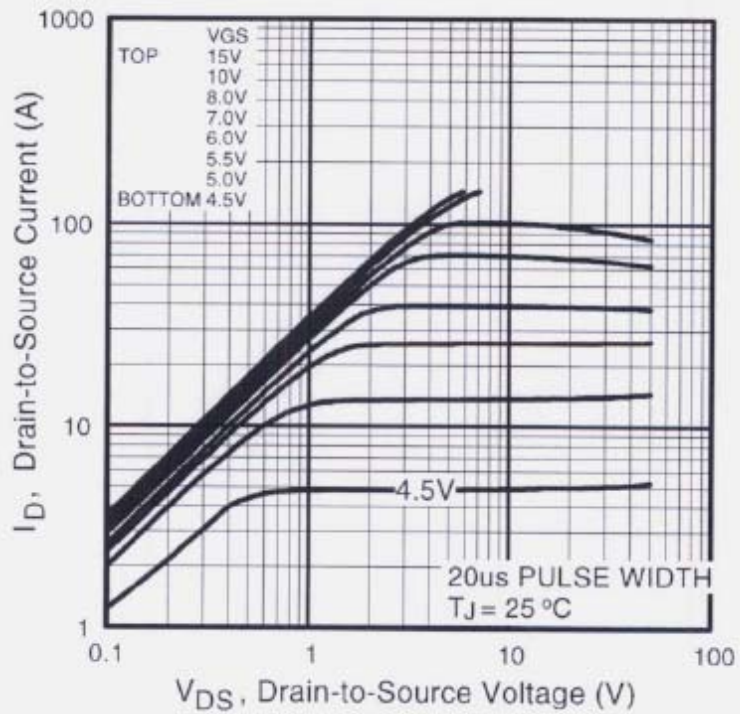


Fig 1. Typical Output Characteristics

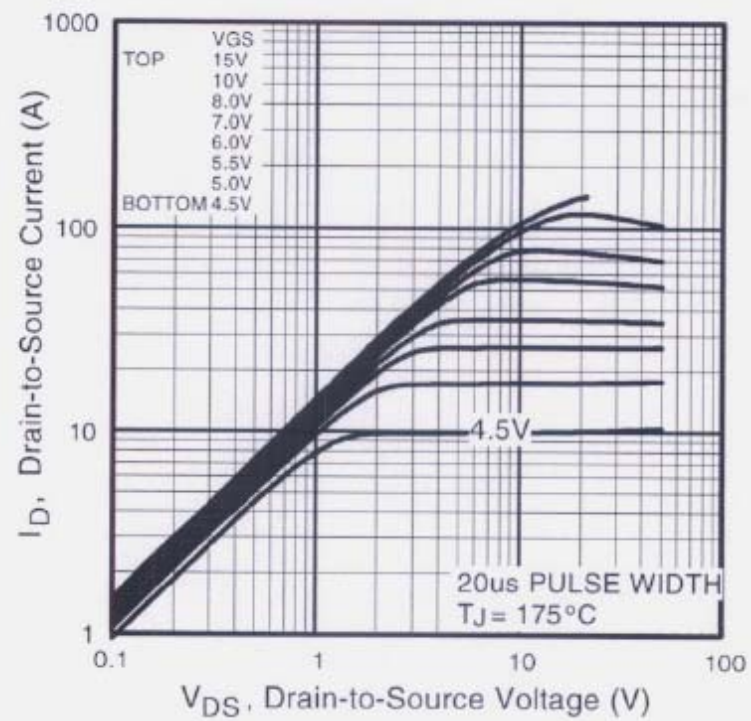
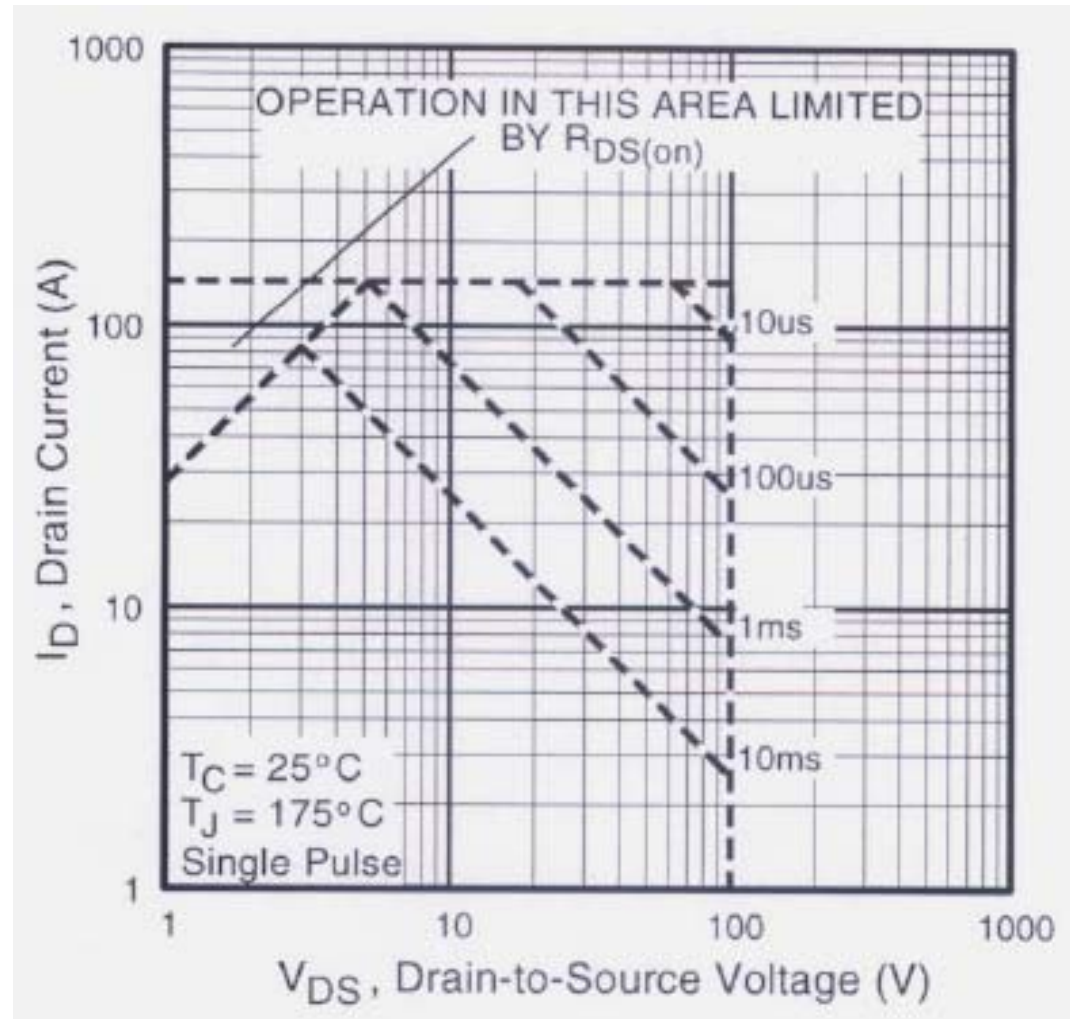
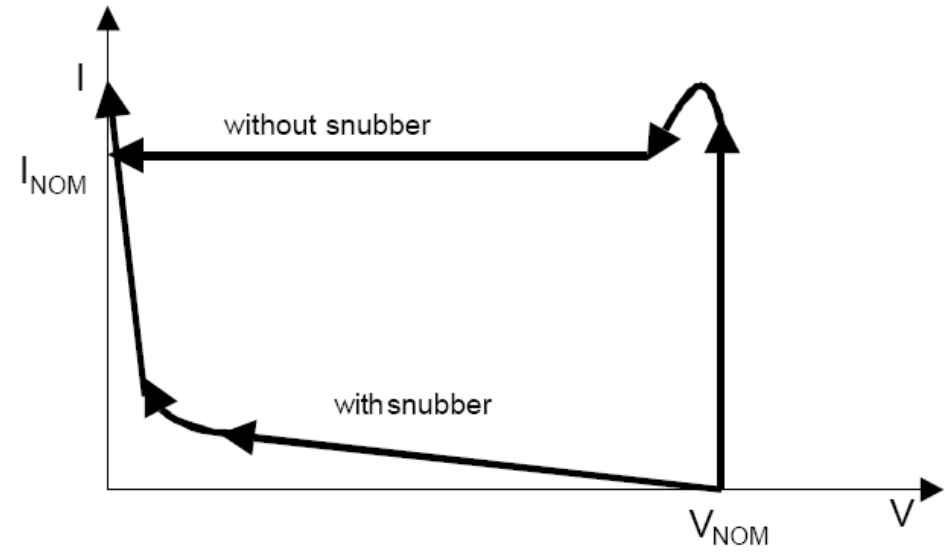
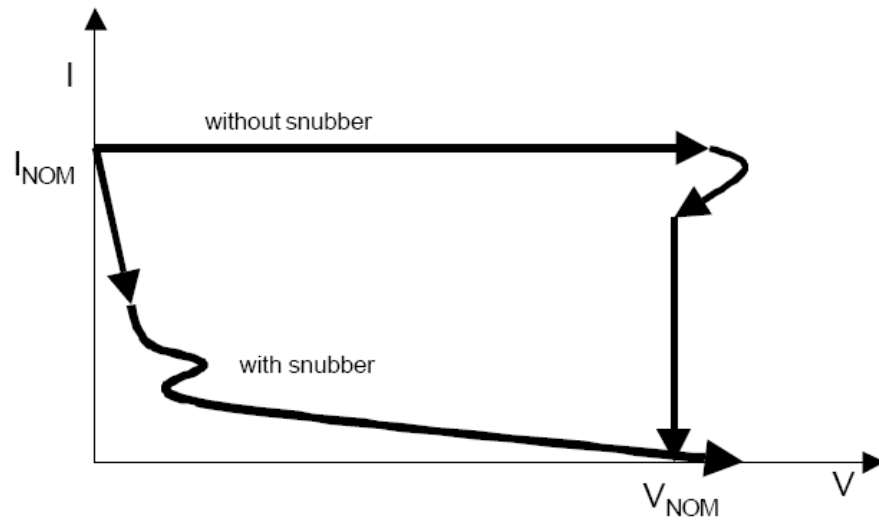
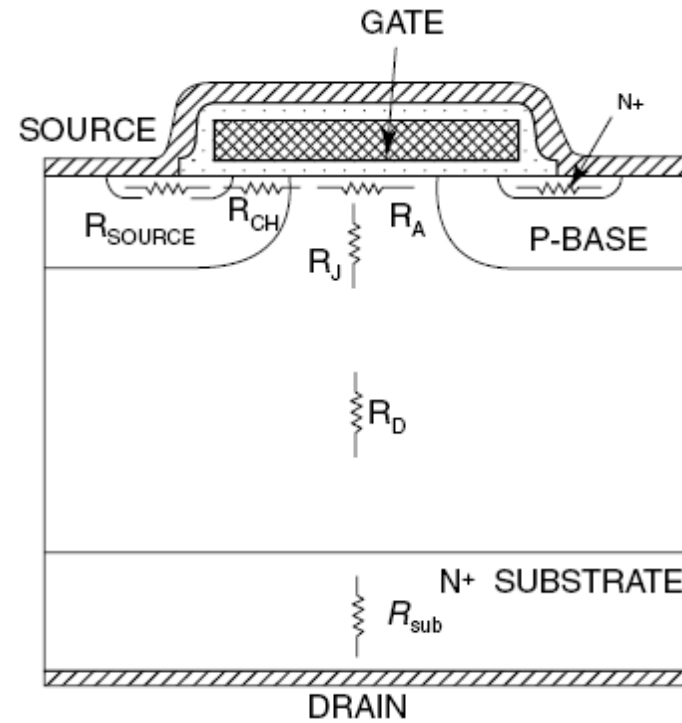
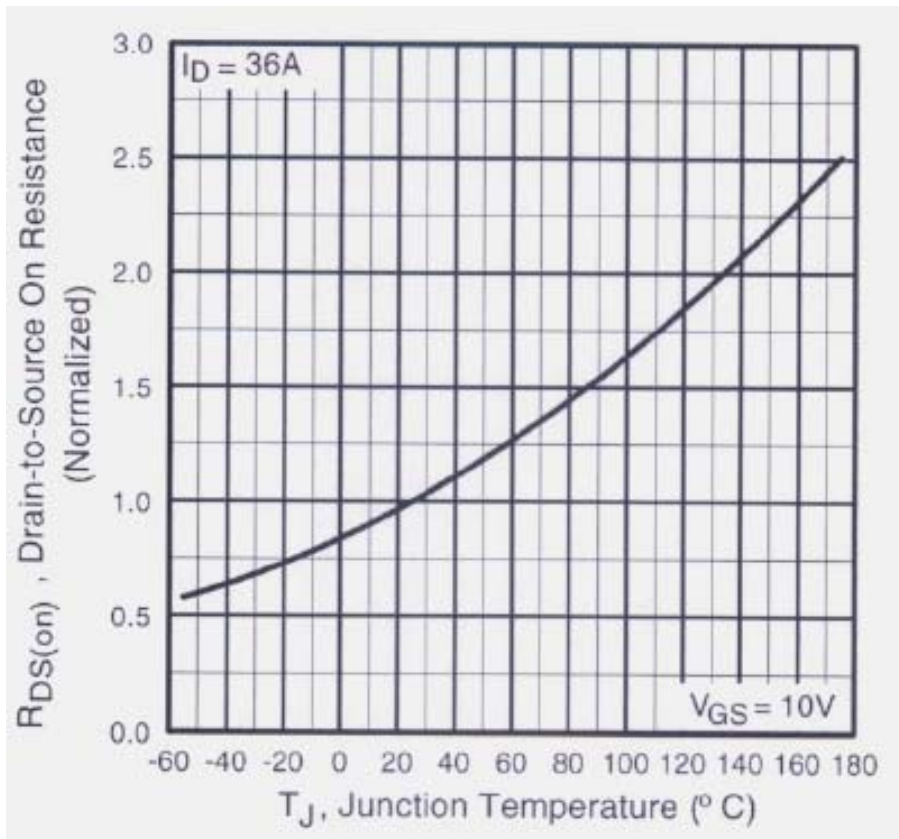


Fig 2. Typical Output Characteristics



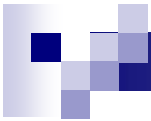


- $R_{DS(on)}$

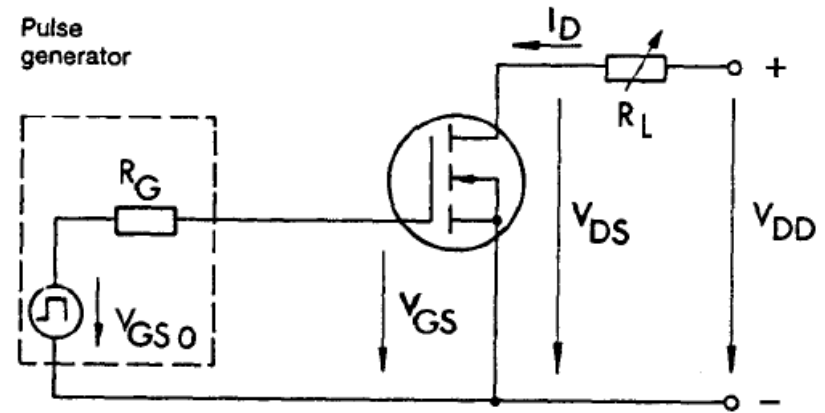
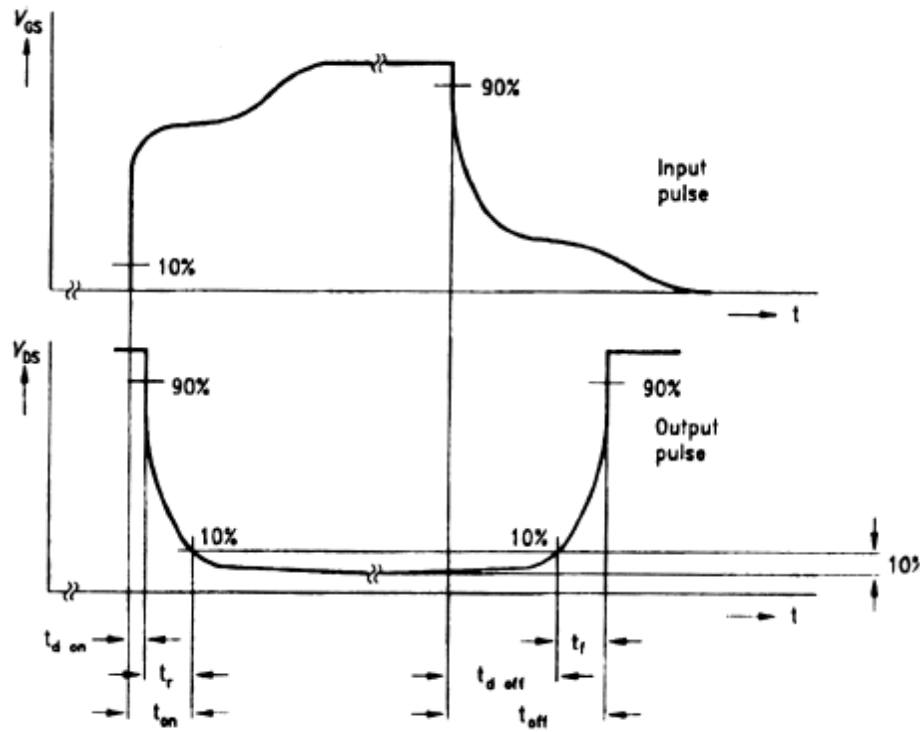


The origin of the internal resistances in a power MOSFET.

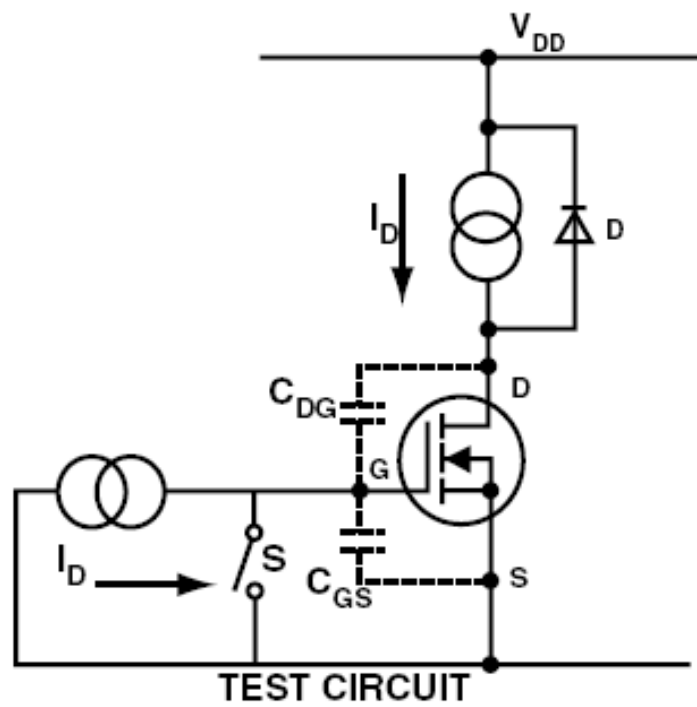
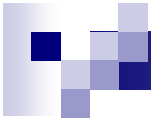
$$R_{dson} = R_{source} + R_{ch} + R_A + R_J + R_D + R_{sub} + R_{wcm1}$$



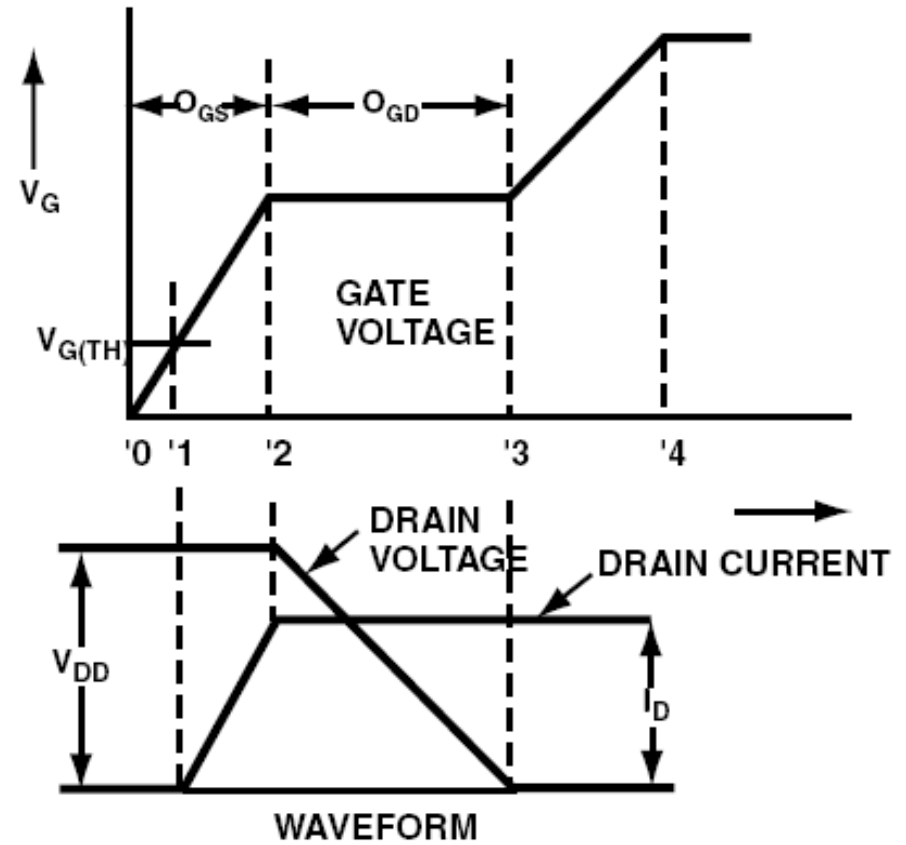
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$t_{d(on)}$	Turn-On Delay Time	—	11	—	ns	$V_{DD} = 50V$
t_r	Rise Time	—	56	—		$I_D = 22A$
$t_{d(off)}$	Turn-Off Delay Time	—	45	—		$R_G = 3.6\Omega$
t_f	Fall Time	—	40	—		$R_D = 2.9\Omega$ See Fig. 10 ④⑤

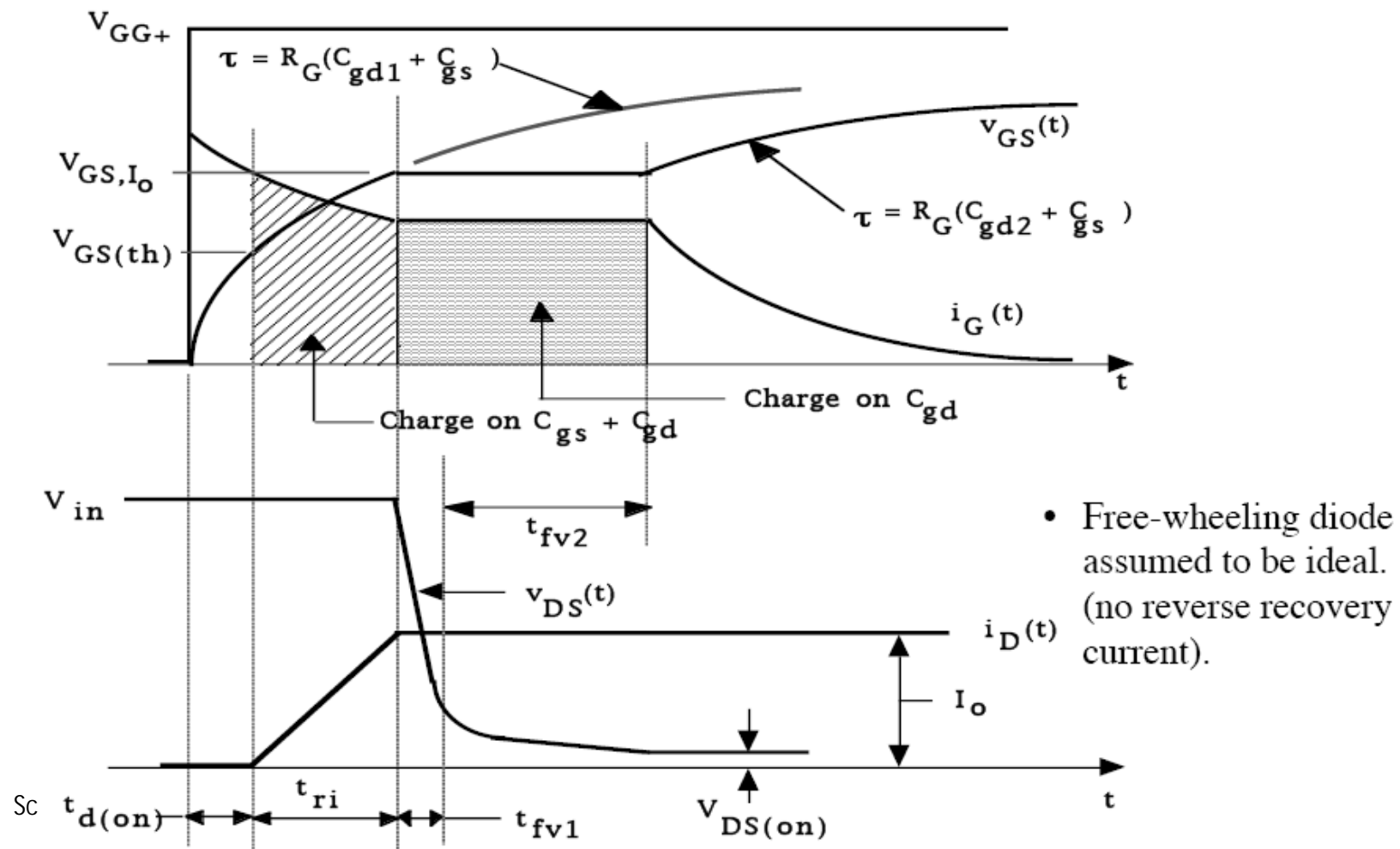


(a)

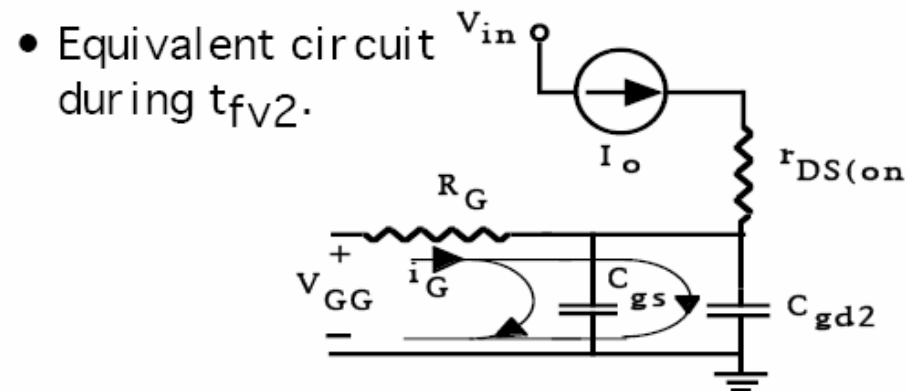
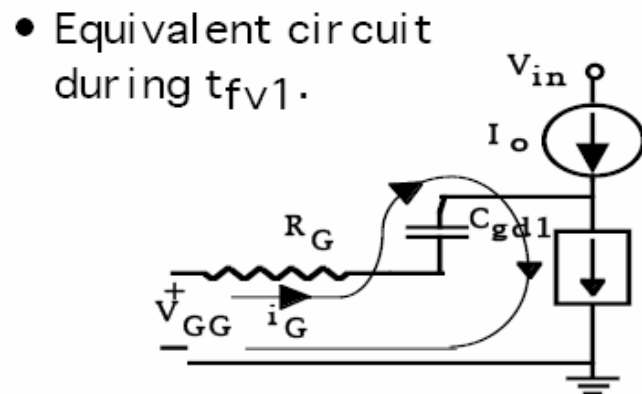
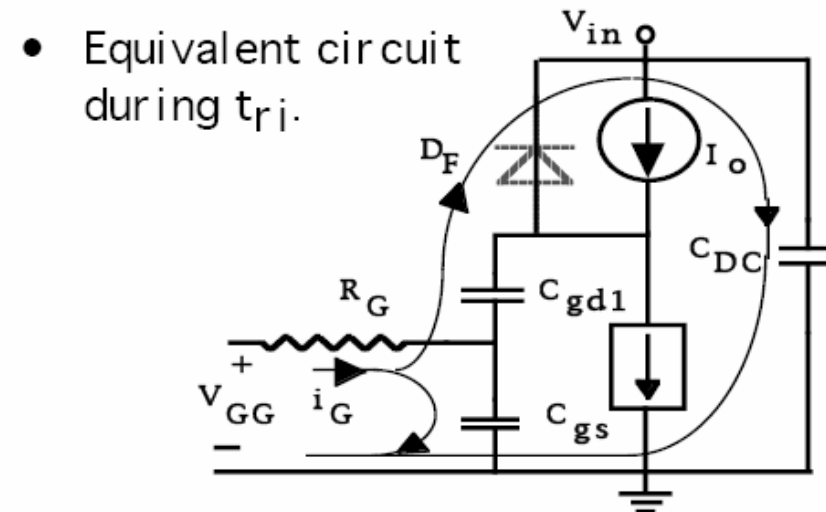
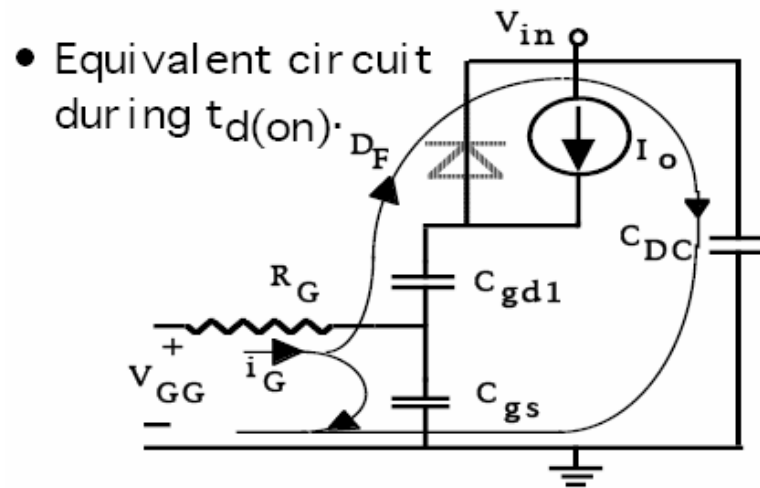


(b)

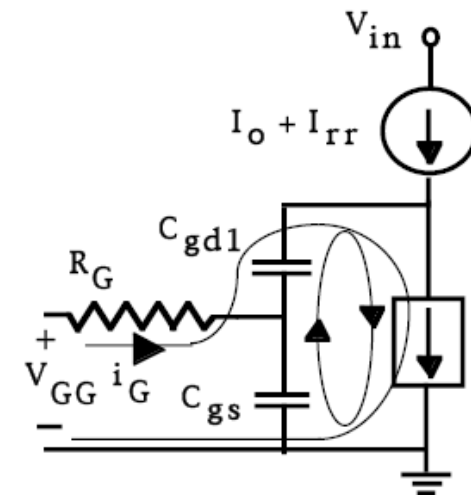
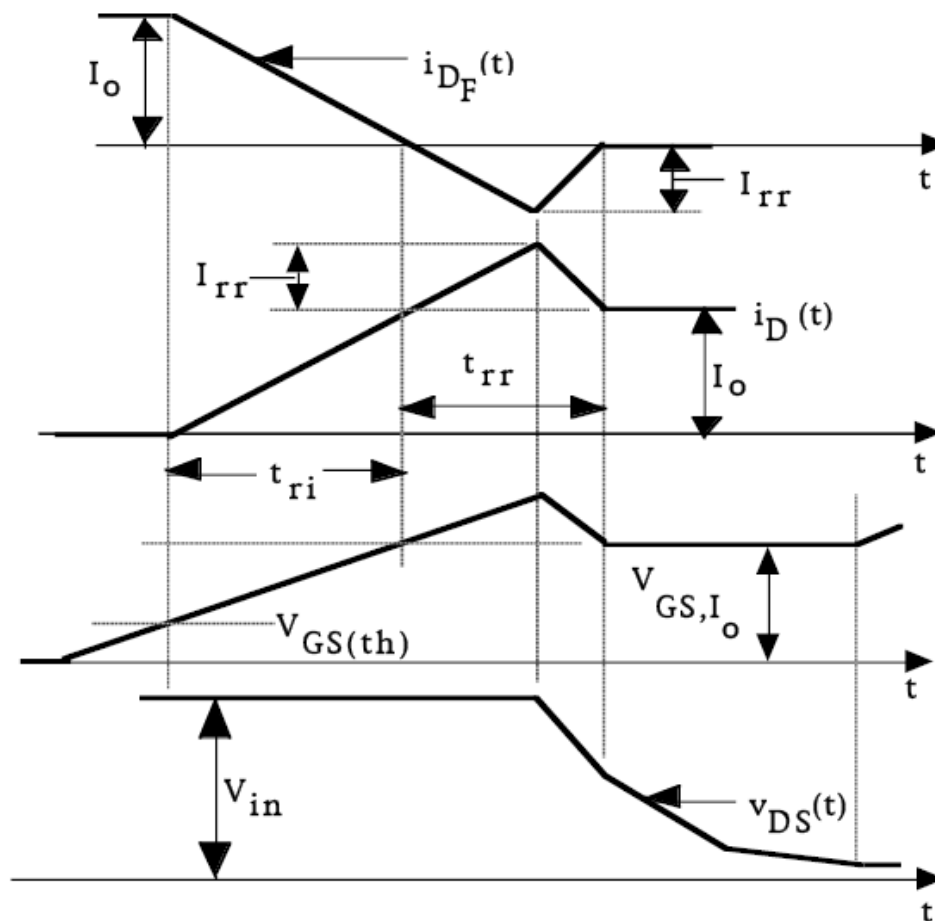
MOSFET-based Buck Converter Turn-on Waveforms



Turn-on Equivalent Circuits for MOSFET Buck Converter

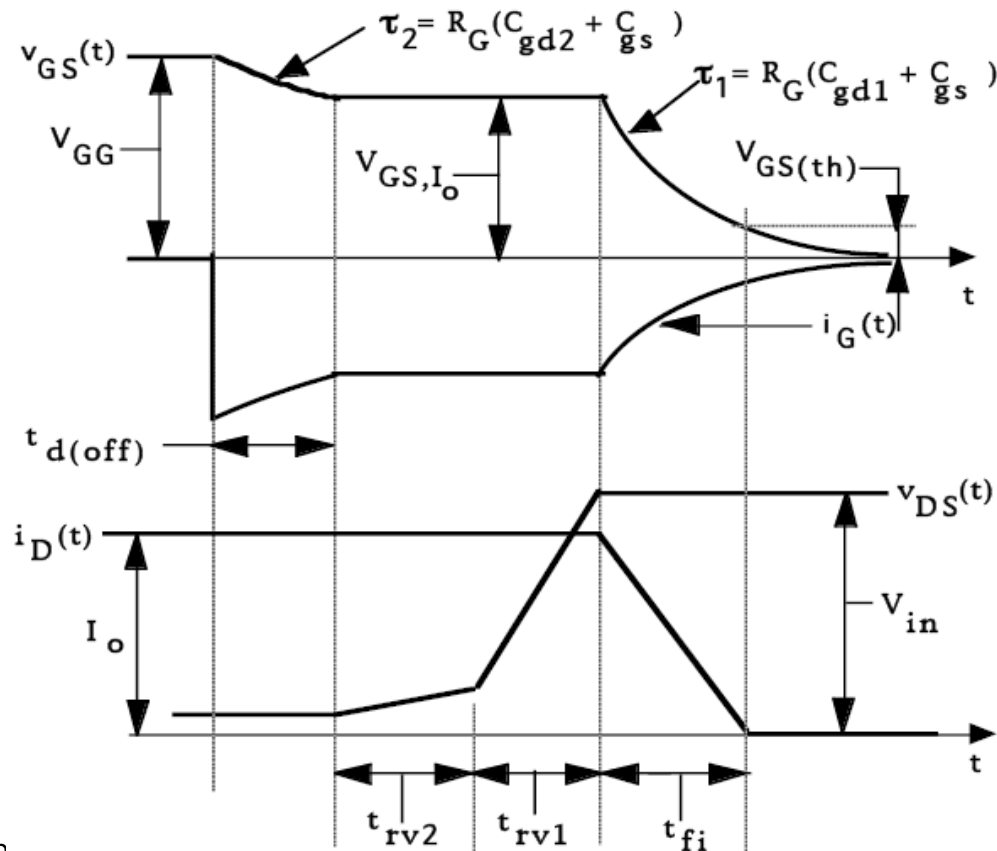


Turn-on Waveforms with Non-ideal Free-wheeling Diode



- Equivalent circuit for estimating effect of free-wheeling diode reverse recovery.

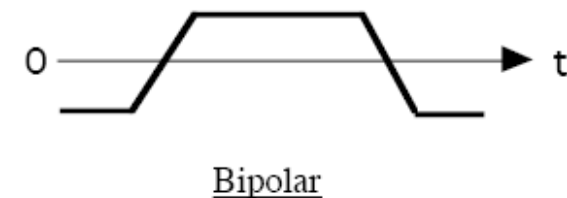
MOSFET-based Buck Converter Turn-off Waveforms



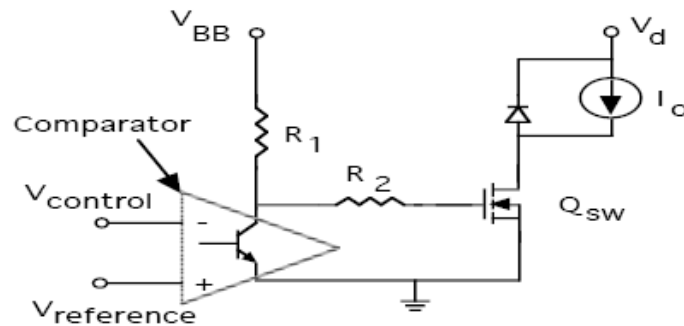
- Assume ideal free-wheeling diode.
- Essentially the inverse of the turn-on process.
- Model quantitatively using the same equivalent circuits as for turn-on. Simply use correct driving voltages and initial conditions

Drive Circuit Design Considerations

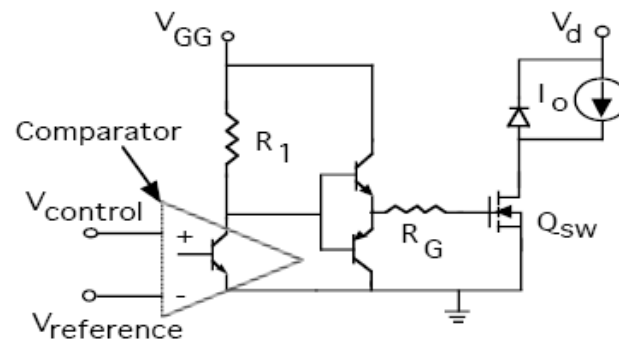
- Drive circuit topologies
 - Output signal polarity - unipolar or bipolar
 - AC or DC coupled
 - Connected in shunt or series with power switch
- Output current magnitude
 - Large I_{on} shortens turn-on time but lengthens turn-off delay time
 - Large I_{off} shortens turn-off time but lengthens turn-on delay time
- Provisions for power switch protection
 - Overcurrents
 - Blanking times for bridge circuit drives
- Waveshaping to improve switch performance
 - Controlled di_B/dt for BJT turn-off
 - Anti-saturation diodes for BJT drives
 - Speedup capacitors
 - Front-porch/backporch currents
- Component layout to minimize stray inductance and shielding from switching noise



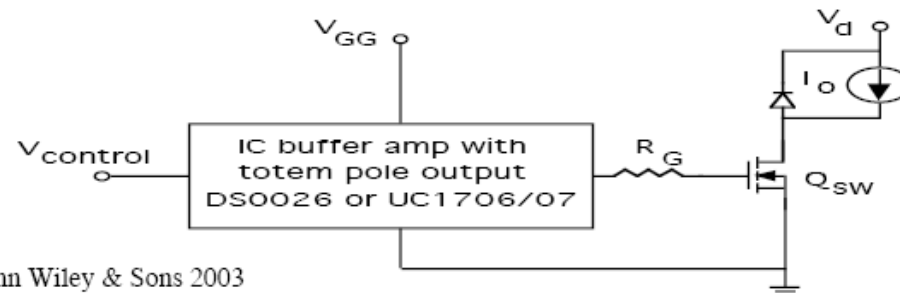
Unipolar DC-coupled Drive Circuits- MOSFET examples



- $V_{\text{control}} > V_{\text{reference}}$
comparator output high and Q_{sw} on
- $V_{\text{control}} < V_{\text{reference}}$
comparator output low and Q_{sw} off



- $V_{\text{control}} > V_{\text{reference}}$
comparator output high putting Q_{npn} on and thus Q_{sw} on
- $V_{\text{control}} < V_{\text{reference}}$
comparator output low putting Q_{pnp} on and thus Q_{sw} off



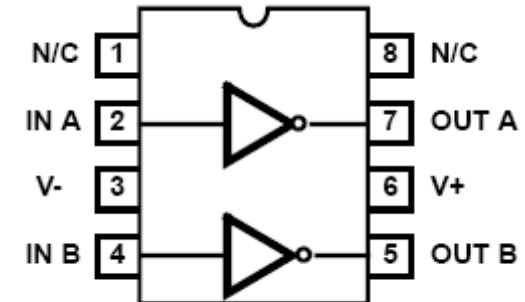
ICL7667

Dual Power MOSFET Driver

Features

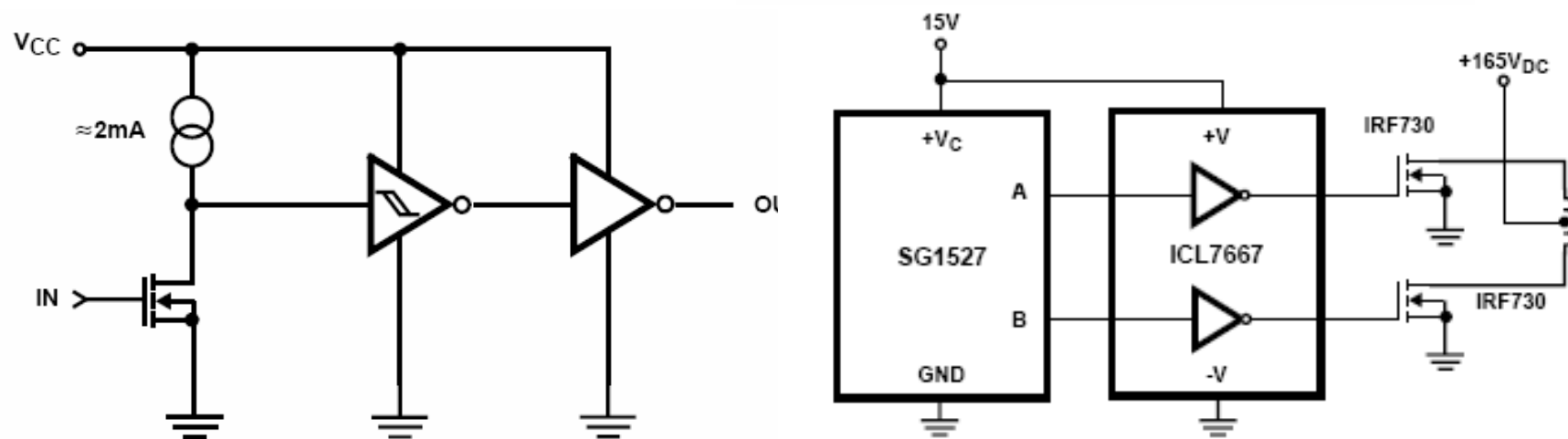
- ◆ Fast Rise and Fall Times – Typically 20ns with 1000pF Load
- ◆ Wide Supply Range: $V_{DD} = 4.5V$ to 17V
- ◆ Low Power Consumption:
6mW with Inputs Low
120mW with Inputs High
- ◆ TTL/CMOS Input Compatible
- ◆ Low R_{OUT} – Typically 4Ω
- ◆ Pin Equivalent to DS0026/DS0056, TSC426, SG1626/SG2626/SG3626

ICL7667

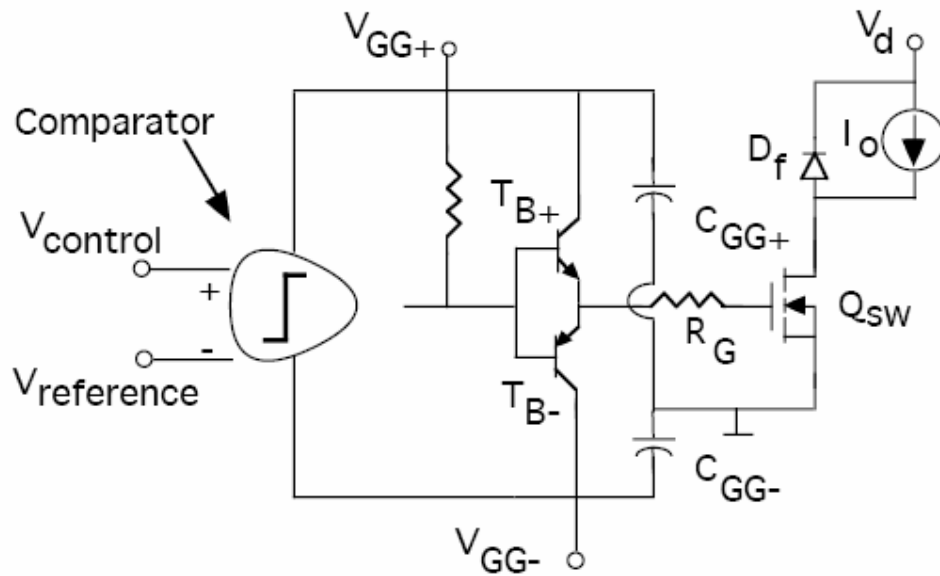


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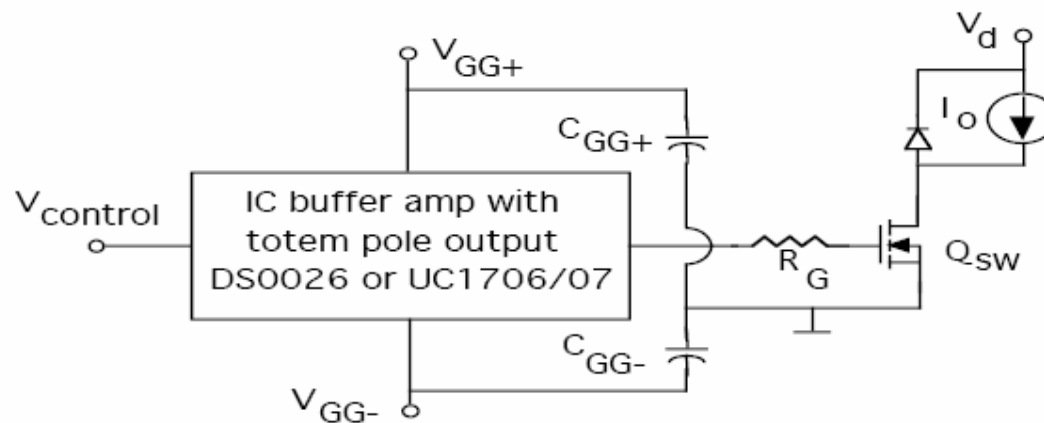
SWITCHING SPECIFICATIONS							
Delay Time	T_{D2}	35	50	-	-	60	ns
Rise Time	T_R	20	30	-	-	40	ns
Fall Time	T_F	20	30	-	-	40	ns
Delay Time	T_{D1}	20	30	-	-	40	ns



Bipolar DC-coupled Drive Circuit- MOSFET Example



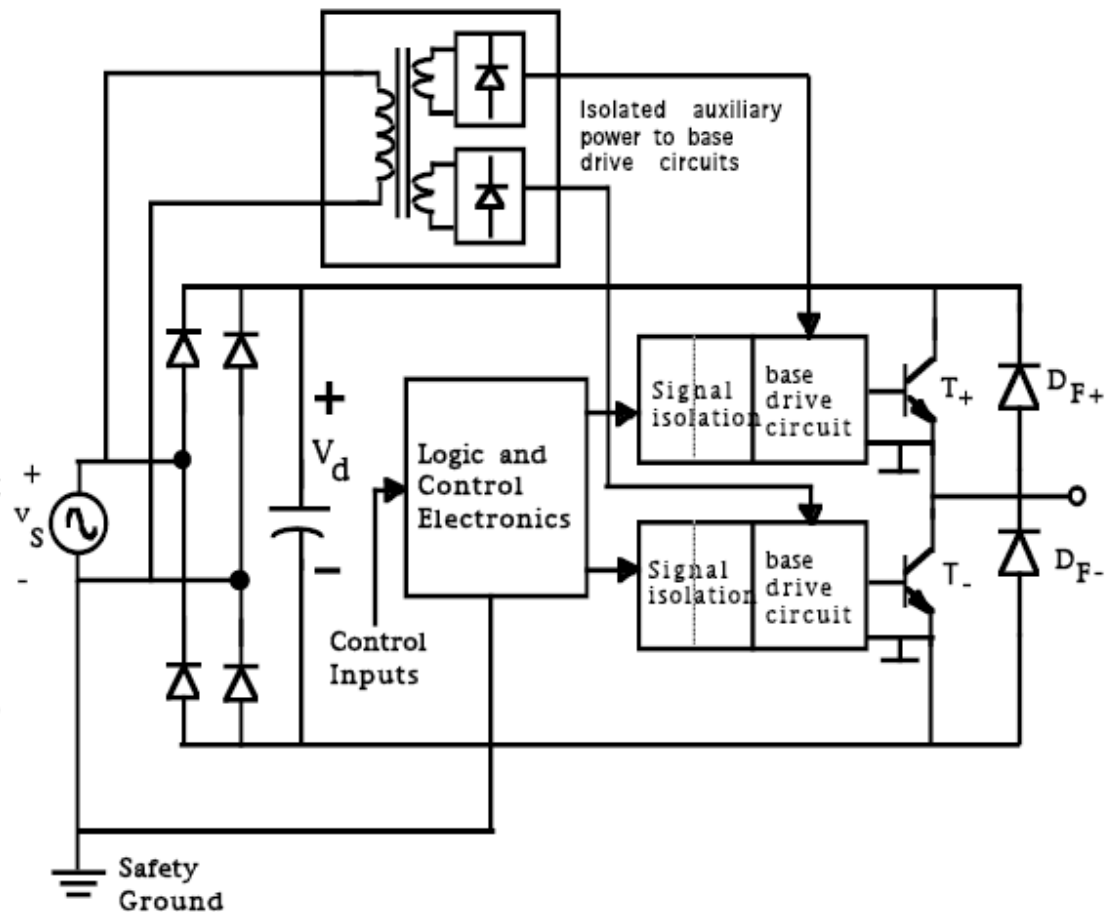
- Bipolar drive with substantial output current capability



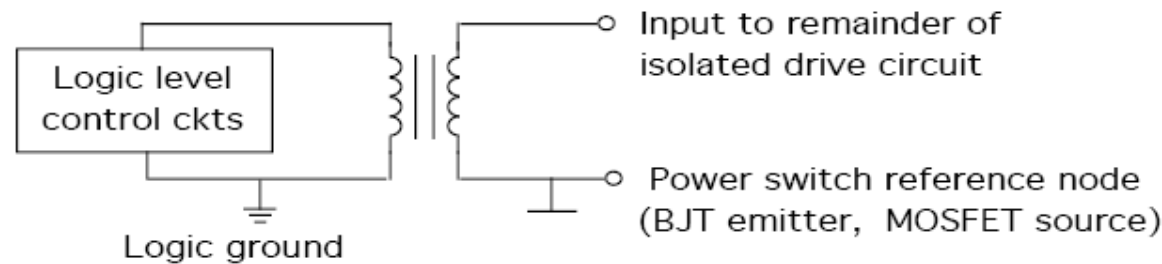
- Simple bipolar drive circuit with moderate (1 amp) output current capability

Need for Electrical Isolation of Drive Circuits

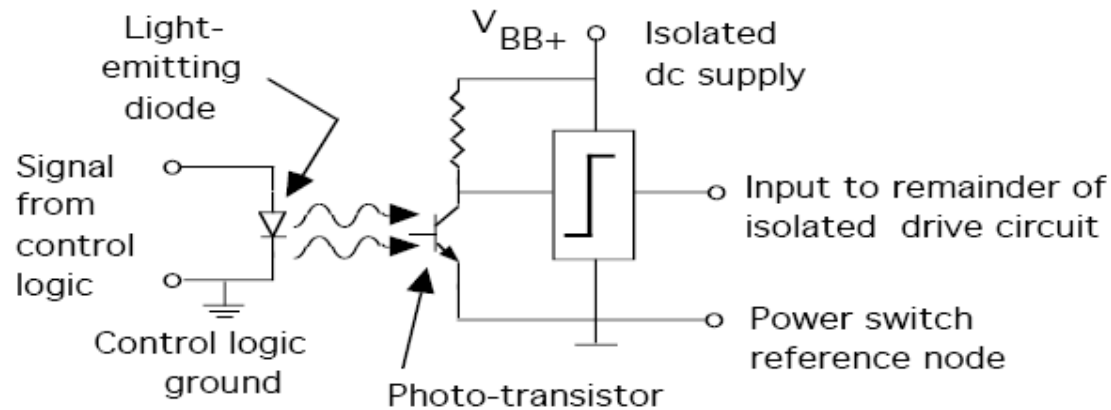
- Negative half cycle of $v_s(t)$ - positive dc rail near safety ground potential. T_- emitter potential large and negative with respect to safety and logic ground
- Positive half cycle of $v_s(t)$ - negative dc rail near safety ground potential. T_+ emitter substantially positive with respect to safety ground if T_- is off
- Variation in emitter potentials with respect to safety and logic ground means that electrical isolation of emitters from logic ground is needed.



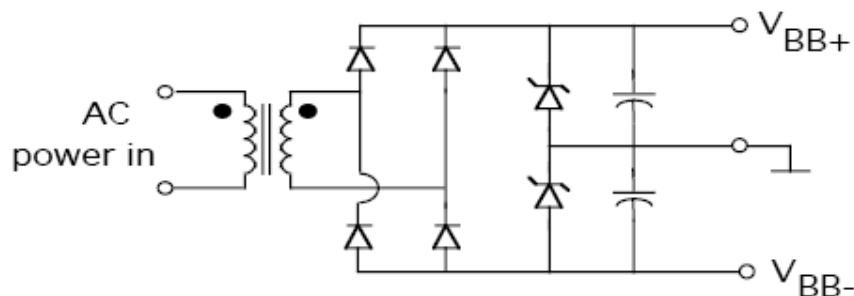
Methods of Control Signal Isolation



- Transformer isolation

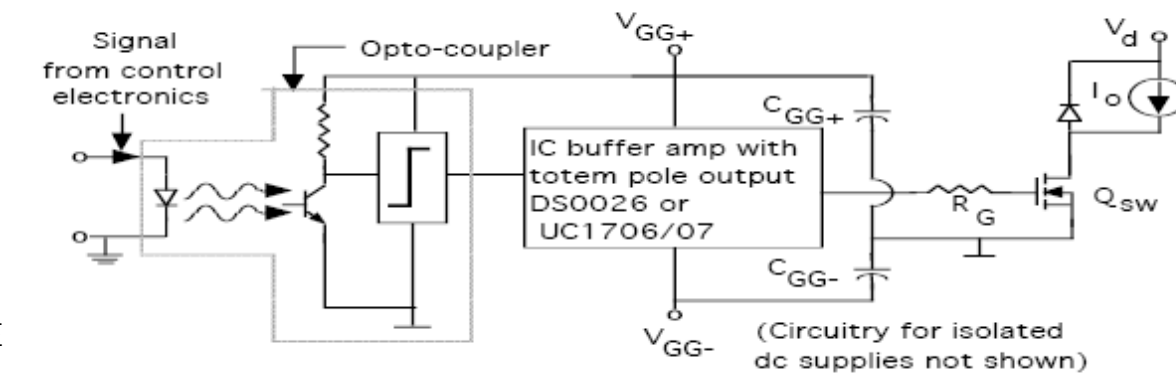
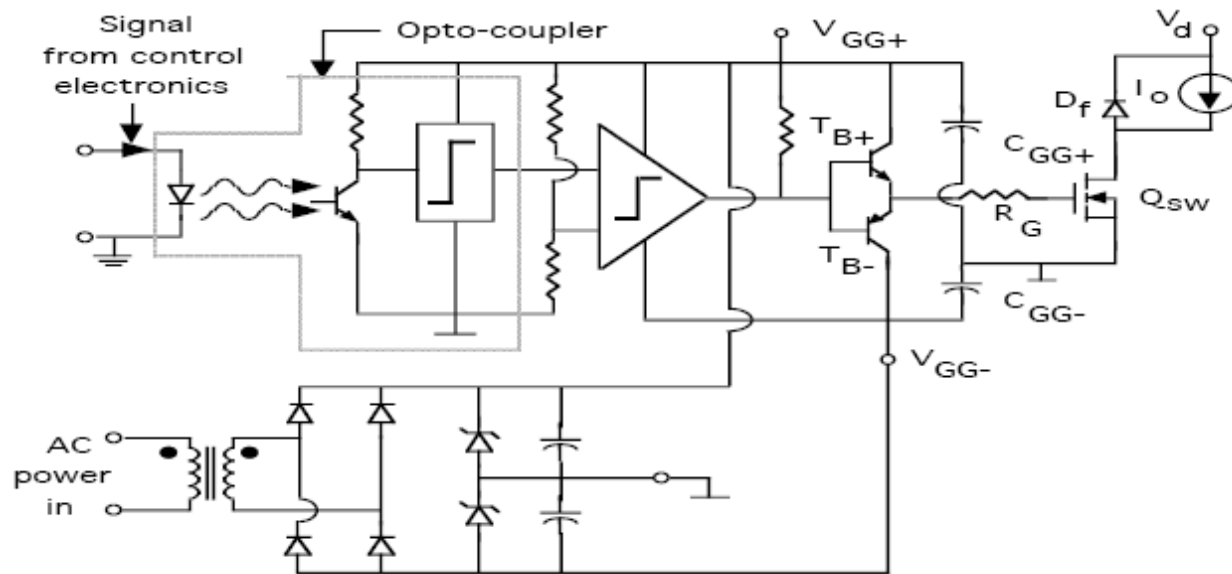


- Opto-coupler isolation

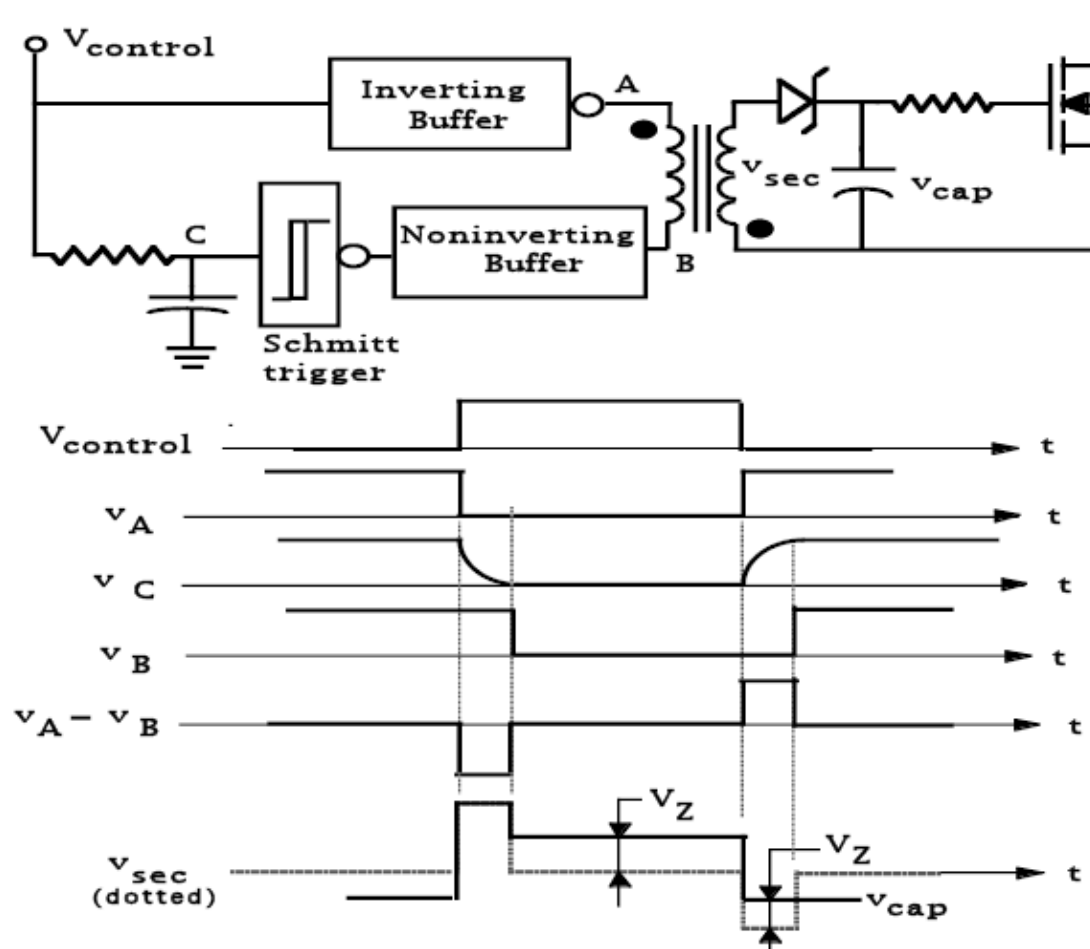


- Isolated dc power supplies for drive circuits

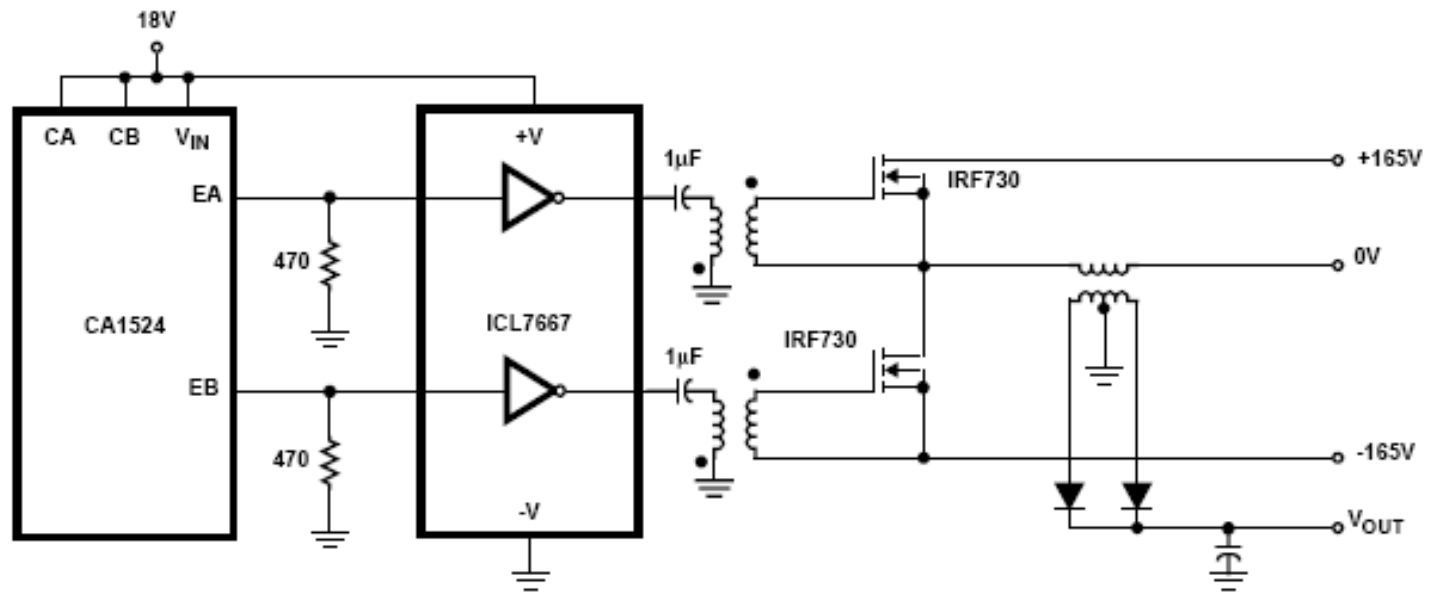
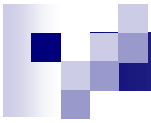
Opto-Coupler Isolated MOSFET Drives



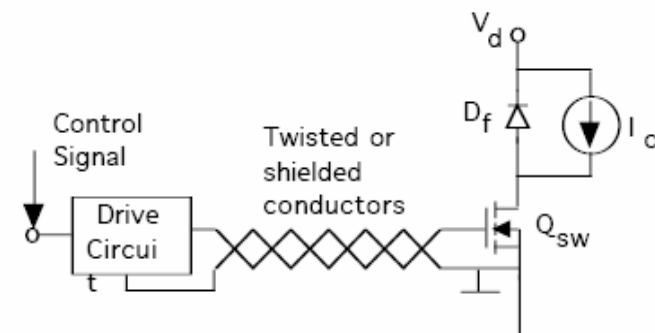
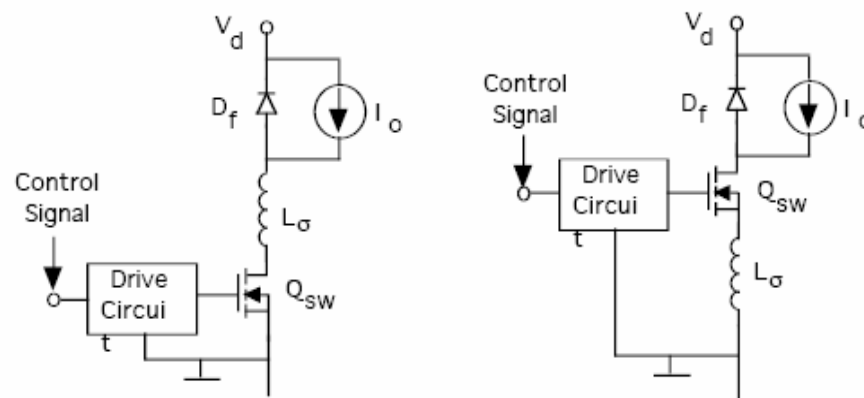
Isolated Drive Without Auxiliary DC Supplies - MOSFET Example



Zener diode voltage V_Z must be less than negative pulse out of transformer secondary or pulse will not reach MOSFET gate to turn it off.



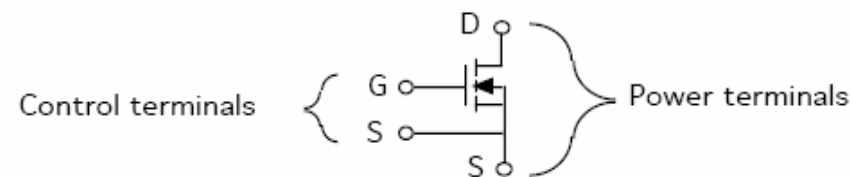
Circuit/Component Layout Considerations



Use shielded conductors to connect drive circuit to power switch if there must be any appreciable separation (few cm or more) between them

Prime consideration is minimizing stray inductance

- Stray inductance in series with high-voltage side of power device Q_{sw} causes overvoltage at turn-off.
- Stray inductance in series with low-voltage side power device Q_{sw} can cause oscillations at turn-on and turn-off.
- One cm of unshielded lead has about 5 nH of series inductance.
- Keep unshielded lead lengths to an absolute minimum.



Some power devices provided with four leads, two input leads and two power leads, to minimize stray inductance in input circuit.